

Distillation Separation Effect by Thermosiphon Reboiler



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PreFEED Corporation

Hiromasa Taguchi

Introduction

- When examining a distillation column using a general-purpose simulator, it is common practice to calculate the condenser and the reboiler as one with the distillation column. This is because the number of recycle loops is reduced, and improvement in convergence can be expected.
- There are roughly two types of classification for reboilers: the kettle type and the thermosiphon type. In the case of a thermosiphon type in which vapor and liquid return to the distillation column in a mixed phase state, the distillation separation effect is difficult to understand.
- In this study, we will create simple distillation column models to examine the distillation separation effect of the thermosiphon type and compare it with the kettle type.

Components:

Methanol (1)

Ethanol (2)

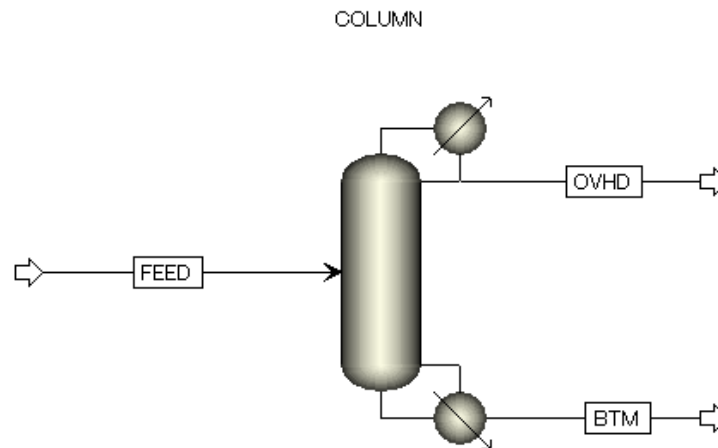
Feed:

Equimolar

Distillation Column

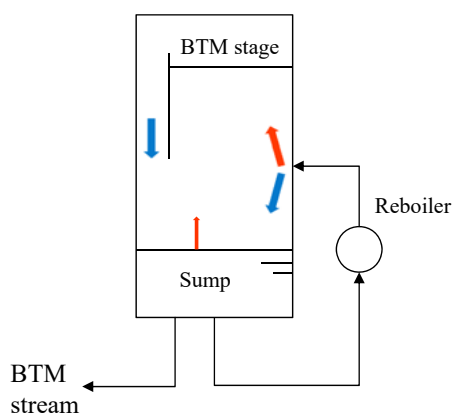
Operating Pressure:

1 ATM

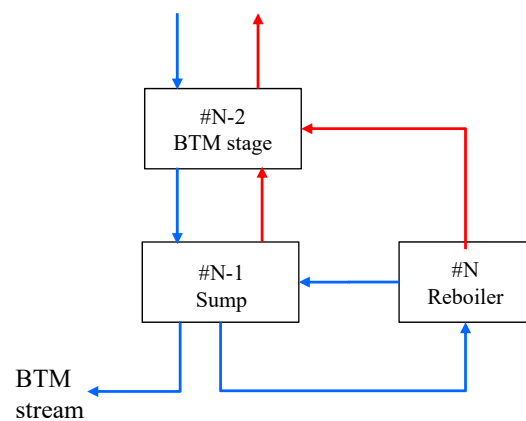


The number of theoretical stages is set to seven so that the impact of the separation effect by the reboiler can be more clearly understood. Also, Aspen Plus is used for the distillation calculation.

Thermosiphon Reboiler Model



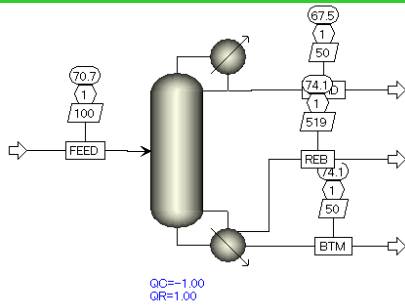
Bottom Section of Actual Distillation Column



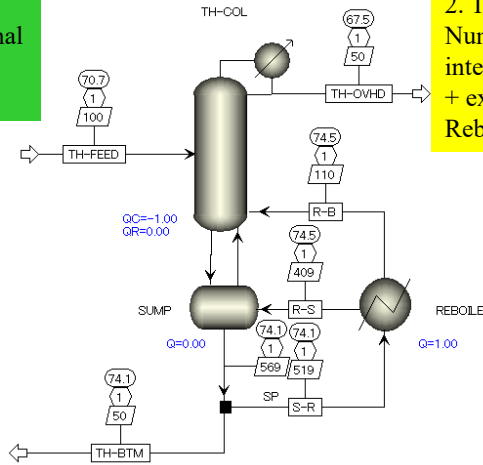
Thermosiphon Reboiler Study Model

The left figure is the equipment configuration around the bottom of the actual distillation column. The right figure is a diagram for verifying the separation effect of the thermosiphon reboiler. The return liquid from the thermosiphon reboiler returns to the sump and the vapor returns to the distillation column BTM stage.

1. Thermosiphon Model A:
 Number of theoretical stages = 7+ (internal condenser & thermosiphon reboiler)
 Reboiler outlet vapor fraction ≈ 0.36



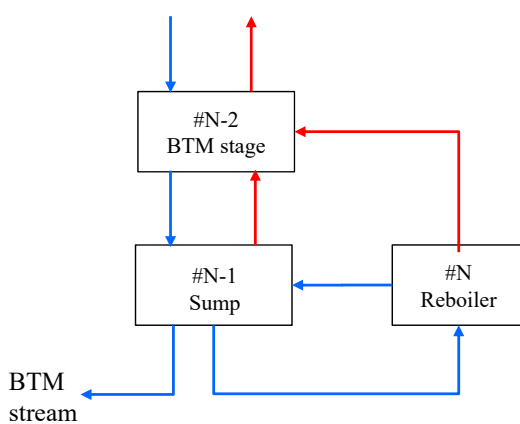
2. Thermosiphon Model B:
 Number of theoretical stages = 7+ internal condenser
 + external sump & reboiler
 Reboiler outlet vapor fraction ≈ 0.36



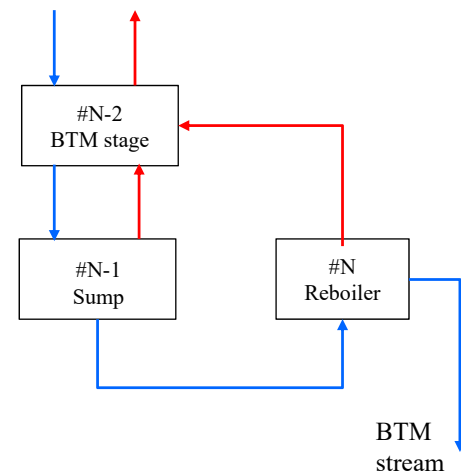
- The results of model A (left figure), in which the distillation column and thermosiphon are calculated together, and model B (right figure), in which the thermosiphon is externally attached, agree with each other.
- It can be seen that the separation effect of thermosiphon can be evaluated by the external model.

| | FEED | OVHD | BTM | TH-OVHD | TH-BTM |
|-------------------|-------|--------|--------|---------|--------|
| Temperature C | 70.7 | 67.5 | 74.1 | 67.5 | 74.1 |
| Pressure bar | 1.013 | 1.013 | 1.013 | 1.013 | 1.013 |
| Mole Flow kmol/hr | 100 | 50 | 50 | 50 | 50 |
| Mole Flow kmol/hr | | | | | |
| MeOH | 50 | 37.073 | 12.927 | 37.073 | 12.927 |
| EtOH | 50 | 12.927 | 37.073 | 12.927 | 37.073 |
| Mole Frac | | | | | |
| MeOH | 0.5 | 0.741 | 0.259 | 0.741 | 0.259 |
| EtOH | 0.5 | 0.259 | 0.741 | 0.259 | 0.741 |

Kettle Type Reboiler Model



Thermosiphon Reboiler Study Model

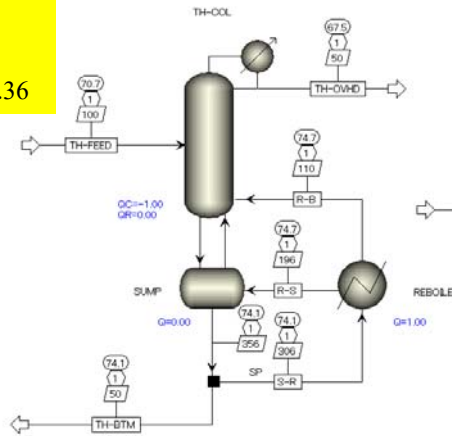


Kettle Type Reboiler Study Model

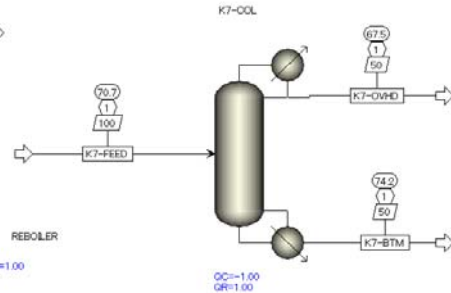
The right figure is a diagram of a kettle type reboiler model. After pool boiling, only steam returns to the distillation tower BTM stage. The separation efficiency is examined using the above model. In this study, the distillate flow rate and the reboiler heat load of the distillation column are set equal in all cases in order to have equal operating conditions.

Thermosiphon versus Kettle

2. Thermosiphon Model B:
 Number of theoretical stages = 7+
 internal condenser
 + (external sump & reboiler)
 Reboiler outlet vapor fraction ≈ 0.36



3. Kettle Type Model:
 Number of theoretical stages = 7 +
 (internal condenser + kettle reboiler)

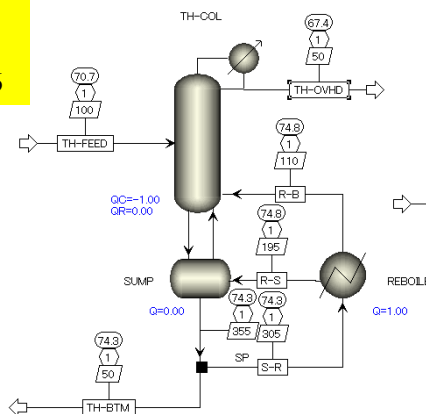


Overhead MeOH
 Concentration
 Thermosiphon: 0.741
 Kettle: 0.745
 The thermosiphon (model B)
 has a poorer separation than
 the kettle type. In other words,
 it can be seen that the effect
 of one theoretical stage
 cannot be expected.

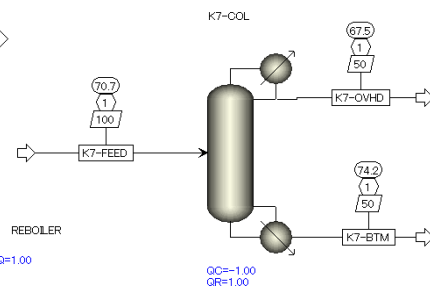
| | FEED | TH-OVHD | TH-BTM | TH-OVHD | TH-BTM |
|-------------------|-------|---------|--------|---------|--------|
| Temperature C | 70.7 | 67.5 | 74.1 | 67.5 | 74.2 |
| Pressure bar | 1.013 | 1.013 | 1.013 | 1.013 | 1.013 |
| Mole Flow kmol/hr | 100 | 50 | 50 | 50 | 50 |
| Mole Flow kmol/hr | | | | | |
| MeOH | 50 | 37.073 | 12.927 | 37.273 | 12.727 |
| EtOH | 50 | 12.927 | 37.073 | 12.727 | 37.273 |
| Mole Frac | | | | | |
| MeOH | 0.5 | 0.741 | 0.259 | 0.745 | 0.255 |
| EtOH | 0.5 | 0.259 | 0.741 | 0.255 | 0.745 |

Thermosiphon versus Kettle -2

2. Thermosiphon Model C:
 Number of theoretical stages = 8+
 internal condenser
 + (external sump & reboiler)
 Reboiler outlet vapor fraction ≈ 0.36

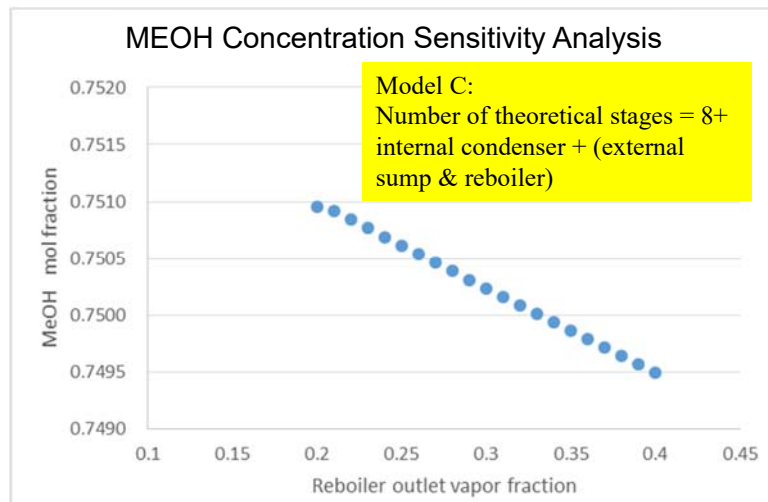


3. Kettle Type Model:
 Number of theoretical stages = 7 +
 (internal condenser + kettle reboiler)



Overhead MeOH
 Concentration
 Thermosiphon: 0.750
 Kettle: 0.745
 In the case where one
 theoretical stage is added to
 model B (model C), the
 thermosiphon has better
 separation.

| | FEED | TH-OVHD | TH-BTM | K7-OVHD | K7-BTM |
|-------------------|-------|---------|--------|---------|--------|
| Temperature C | 70.7 | 67.4 | 74.3 | 67.5 | 74.2 |
| Pressure bar | 1.013 | 1.013 | 1.013 | 1.013 | 1.013 |
| Mole Flow kmol/hr | 100 | 50 | 50 | 50 | 50 |
| Mole Flow kmol/hr | | | | | |
| MeOH | 50 | 37.489 | 12.511 | 37.273 | 12.727 |
| EtOH | 50 | 12.511 | 37.489 | 12.727 | 37.273 |
| Mole Frac | | | | | |
| MeOH | 0.5 | 0.750 | 0.250 | 0.745 | 0.255 |
| EtOH | 0.5 | 0.250 | 0.750 | 0.255 | 0.745 |



- It was found that the separation effect changes according to the outlet vapor fraction as a result of conducting a sensitivity analysis regarding the outlet vapor fraction change of the thermosiphon reboiler.
- Since the circulation rate of the thermosiphon reboiler is determined by the pressure balance, it can be seen that the outlet vapor fraction varies according to the pressure loss, and that the separation efficiency changes as a result.

Conclusion

- In this case study, the separation effect of a thermosiphon reboiler was discussed in comparison with a kettle type reboiler.
- Vertical thermosiphons are often preferred in new plant distillation columns due to advantages such as their smaller footprints. However, a thermosiphon is inefficient because liquid is recycled, so unlike a kettle type reboiler, it cannot be expected to have the separation effect of one theoretical stage.
- In the case of a thermosiphon, the separation effect changes depending on the circulation rate, but it is generally considered that there is a contribution of about 0.1 to 0.3 theoretical stages. For this reason, it is considered practical (safe) to consider adding one stage in combination with the bottom stage of the distillation column when carrying out distillation studies and the like.